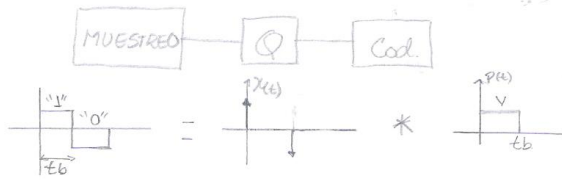


Saranyas, 26/02/04.  
COMUNICACIONES I

MODULACIÓN DIGITAL.



NO RETORNO A CERO  
BIPOLAR.

$$R_x(t) = \sum \frac{R_n}{t_b} S(\bar{c} + nt_b)$$

$$R_n = \lim_{T \rightarrow \infty} \frac{1}{T} \sum_k a_k \Delta t_k$$

$$R_0 = \frac{1}{2}$$

$$R_1 = \begin{cases} 10 = 0 \\ 01 = 0 \\ 11 = 1 \\ 00 = 0 \end{cases} \Rightarrow R_1 = \frac{1}{4} = R_n = \frac{1}{4}$$

Supo. para los códigos unipolares:

$$R_x(t) = \frac{1}{2t_b} S(t) + \sum_{n \neq 0} \frac{1}{4t_b} S(\bar{c} + nt_b) = \frac{1}{2t_b} S(t) + \sum_{\substack{n \\ n \neq 0}} \frac{1}{4t_b} S(\bar{c} + nt_b) - \frac{1}{4t_b} S(t)$$

$$= \frac{1}{4t_b} S(t) + \sum \frac{1}{4t_b} S(\bar{c} + nt_b) \xrightarrow{F} \frac{1}{4t_b} + \frac{1}{4t_b} \cdot \frac{1}{t_b} \sum \delta(f + n f_b) = G_x(f)$$

• CASO NRZ.

• CASO RZ.

$P(f) = |P(f)| e^{j\phi(f)}$  Siempre da cero los productos con  $G_x$ , porque don  $\text{Sinc}(nt_b) = 0$ , menos en caso que de 1 (\*)

• CASO NRZ UNIPOLAR  $\rightarrow |P(f)|^2 = (Nt_b)^2 \text{Sinc}^2 f t_b$  (multiplico  $|P(f)|^2 \cdot G_x(f)$ )

$$= G_x(f) = \frac{V^2 t_b}{4} \text{Sinc}^2 f t_b + \frac{V^2 t_b^2}{4 t_b^2} S(f)$$

Para hallar la potencia total, solo integrar  $G_x(f)$

$$\text{Para } A t_b \text{Sinc}^2 f t_b \Rightarrow \int |x(t)|^2 dt = \frac{\int |P(f)|^2 df}{(Nt_b)^2 \text{Sinc}^2 f t_b} = V^2 t_b \Rightarrow \int t_b \text{Sinc}^2 f t_b = 1$$

PAC = Potencia AC =  $\frac{V^2}{4}$

PDC = Potencia DC =  $\frac{V^2}{4}$

⇒ Potencia total  $\frac{V^2}{2}$

• CASO RZ → UNIFORME → 

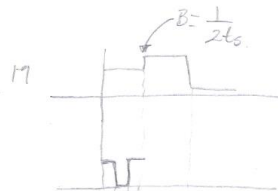
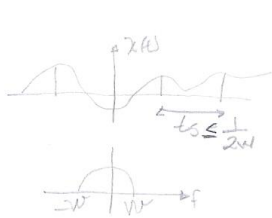
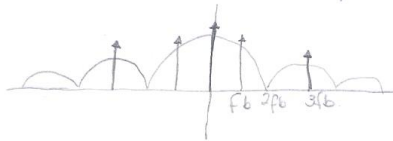
$G_x = F \left\{ \frac{1}{4T_b} \delta(f) + \sum \frac{1}{4T_b} \delta(f \pm n/T_b) \right\} \Rightarrow$  La misma  $G_x$  que en NRZ porque ambas con UNIFORMES

$|P(f)|^2 = \frac{V^2 T_b^2}{4} \text{sinc}^2 f \frac{T_b}{2}$  ,  $G_x(f) = \frac{1}{4T_b} + \sum \frac{1}{4T_b} \delta(f \pm n/T_b)$

$G_y(f) = \frac{V^2 T_b}{16} \text{sinc}^2 f \frac{T_b}{2} + \frac{V^2 T_b^2}{16 T_b^2} \delta(f) + \frac{V^2 T_b^2 \text{sinc}^2 \frac{1}{2} \frac{1}{4T_b} \delta(f \pm n/T_b)}{4} + \frac{V^2 T_b^2 \text{sinc}^2 \frac{3}{2} \frac{1}{4T_b} \dots}{4}$

$\downarrow$   $n=0$                        $\downarrow$   $n=1$                        $n=2 \Rightarrow 0$                        $\downarrow$   $n=3$

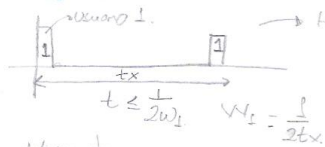
$G_y(f) = \frac{V^2 T_b}{16} \text{sinc}^2 f \frac{T_b}{2} + \frac{V^2}{16} \delta(f) + \sum_{\text{harm.}} \frac{V^2 T_b^2 \text{sinc}^2 \frac{n}{2} \frac{1}{4T_b^2} \delta(f \pm n/T_b)}{4}$



$f_s$  debe cumplir Nyquist.

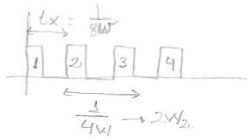
$f_b = \frac{1}{T_b} = \frac{1}{T_s} \Rightarrow f_b = 3f_s \Rightarrow$  el ancho de banda grab.

**MULTIPLEXAJE:**



→ Hay espacio para más usuarios.

USUARIO 1 →  $W_1$   
USUARIO 2 →  $2W_1$



$B = \frac{1}{2tx} = \frac{1}{2 \cdot \frac{1}{8W}} = 4W$